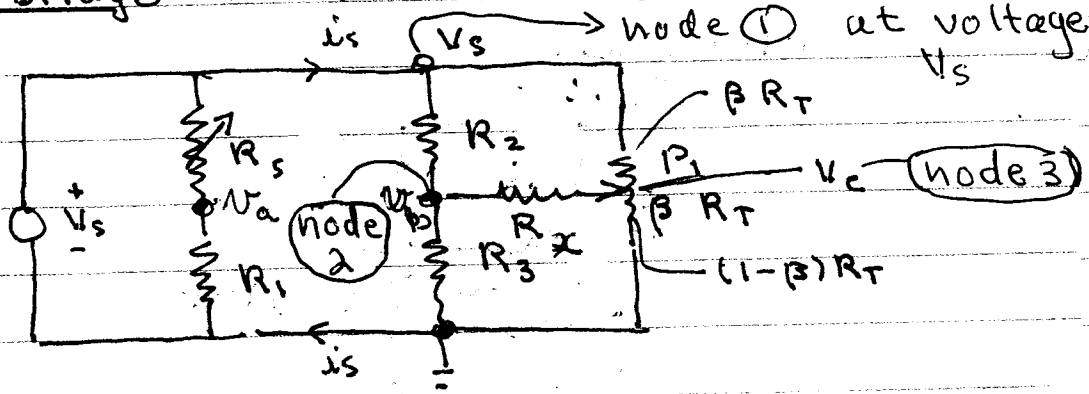


Note on Lab (2) Equation page (3)

Full Bridge Alternative to Δ -Y transform



node equations

node ① KCL $i_s - \frac{V_s - U_b}{R_2} - \frac{V_s - V_c}{\beta R_T} = 0$ — gives i_s in terms of V_s, U_b & V_c

node ② KCL $\frac{U_b - V_s}{R_2} + \frac{U_b - V_c}{R_x} + \frac{U_b}{R_3} = 0$

node ③ KCL $\frac{V_c - V_s}{\beta R_T} + \frac{V_c - U_b}{R_x} + \frac{V_c}{(1-\beta)R_T} = 0$ } give U_b and V_c

③ gives $V_c = \left(\frac{V_s}{\beta R_T} + \frac{U_b}{R_x} \right) / \left(\frac{1}{\beta R_T} + \frac{1}{R_x} + \frac{1}{(1-\beta)R_T} \right)$
 $= \left(\frac{V_s}{\beta R_T} + \frac{U_b}{R_x} \right) / \left(\frac{R_x + \beta R_T(1-\beta)}{R_x \beta R_T(1-\beta)} \right)$

sub in ② to obtain U_b

$$\left(\frac{1}{R_2} + \frac{1}{R_2} + \frac{1}{R_3} \right) U_b = \left(\frac{V_s}{R_2} + \frac{V_c}{R_x} \right)$$

Let $R = R_2 = R_3 = R_{net} = R$

Then

$$\left(\frac{2}{R} + \frac{1}{R_x} \right) U_b = \left(\frac{V_s}{R} + \frac{1}{R_x} \left[\frac{V_s}{\beta R_T} + \frac{U_b}{R_x} \right] \right) / \left(\frac{R_x + \beta(1-\beta)R_T}{R_T R_x \beta(1-\beta)} \right)$$

$$U_b \left(\frac{2}{R} + \frac{1}{R_x} - \frac{1}{R_x^2} \frac{R_x \beta(1-\beta)R_T}{R_x + \beta(1-\beta)R_T} \right) = V_s \left(\frac{1}{R} + \frac{(1-\beta)}{R_x + \beta(1-\beta)R_T} \right)$$

or $\frac{U_b}{V_s} \left(\frac{(R_x + \beta(1-\beta)R_T)(2R_x + R) - R_T \beta(1-\beta)}{R R_x (R_x + \beta(1-\beta)R_T)} \right) = \left(\frac{1}{R} + \frac{(1-\beta)}{R_x + \beta(1-\beta)R_T} \right)$

Thus

$$\frac{V_b}{V_s} = \frac{2R_x^2 + R_x R + 2R_x \beta(1-\beta)R_T}{R_x (R_x + \beta(1-\beta)R_T)}$$
$$= \frac{R_x + \beta(1-\beta)R_T + R(1-\beta)}{R(R_x + \beta(1-\beta)R_T)}$$

Thus

$$\frac{V_b}{V_s} = \frac{(1-\beta)R^{R_{ref}} + \beta(1-\beta)R_T + R_x}{R + 2R_x + 2\beta(1-\beta)R_T}$$

V_a found simply by a voltage divider relation

$$V_a = \frac{R_1}{R_1 + R_s} \times V_s$$

Note: have used

R_1 for R_{ref} , etc
and then assumed

$$\dots R_2 = R_3$$